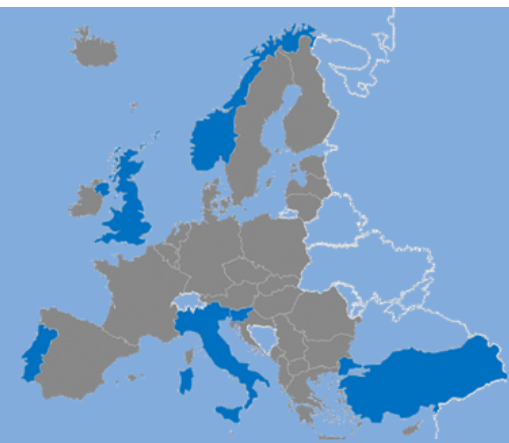




European
Commission

Horizon 2020
European Union funding
for Research & Innovation

liquefACT



EARTHQUAKE INDUCED LIQUEFACTION RISK: HOLISTIC ASSESSMENT AND MITIGATION

Wednesday 20th June 2018 - 11:30-13:00

ROOM: CR2 (building M2 - Thessaloniki Concert Hall/16ECEE
Conference Venue)



*Liquefaction vulnerability of structures
and infrastructures on liquefiable deposits*

Maxim Millen, Xavier Romão

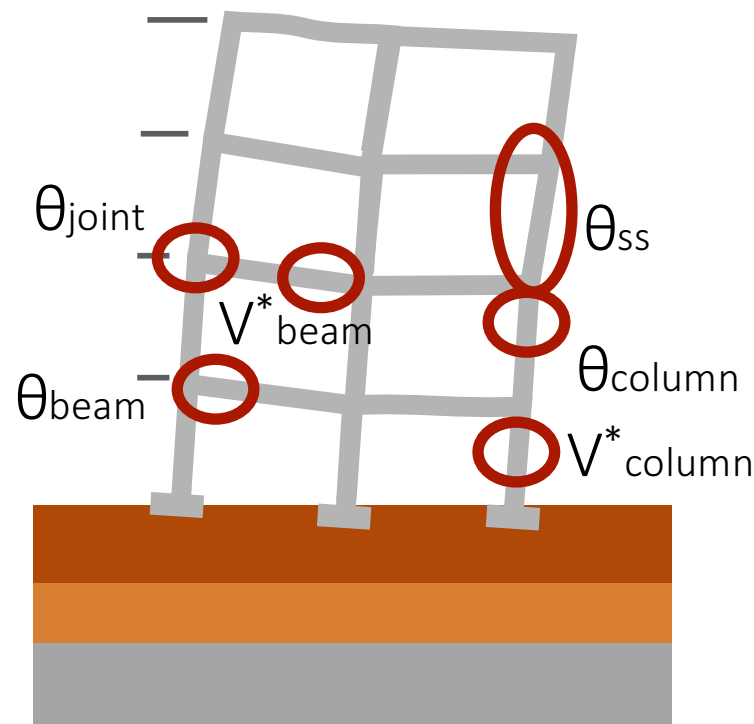
UNIVERSITY OF PORTO

U.PORTO
FEUP FACULDADE DE ENGENHARIA
UNIVERSIDADE DO PORTO

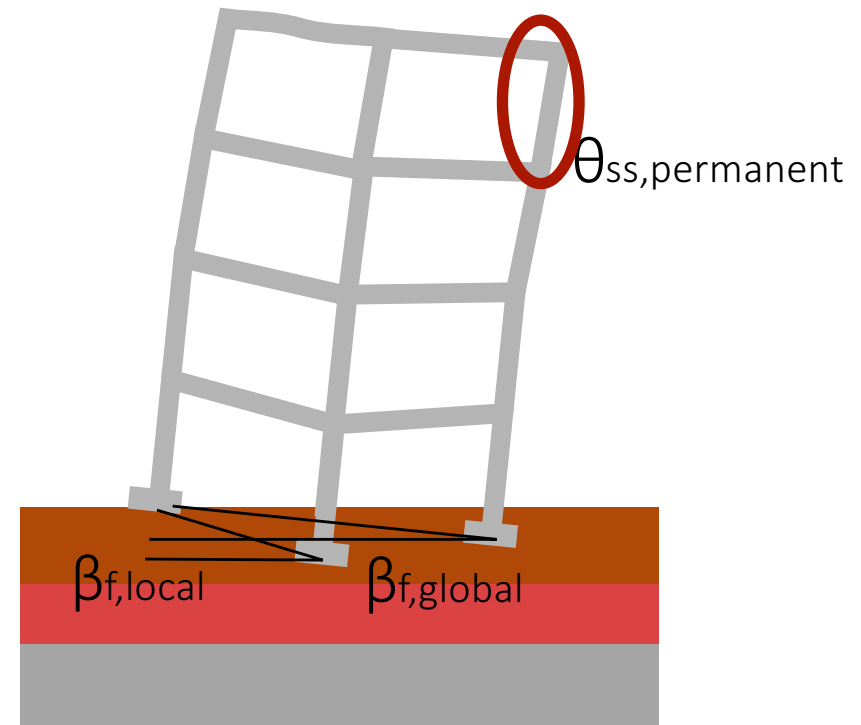
OUTLINE

- Goal
- Equivalent soil profiles
- Procedure to assess performance
- Moment-rotation response
- From soil to structure (Xavier Romão to continue)

Quantifying performance of buildings on liquefiable soil



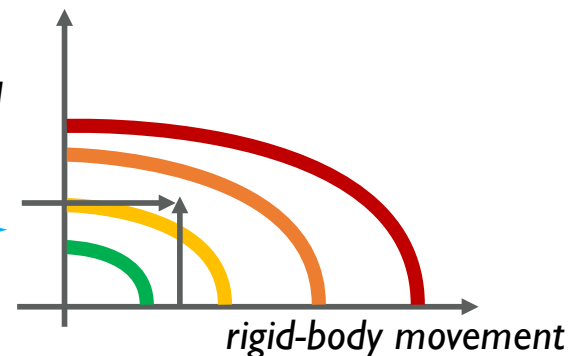
Dynamic performance



Residual performance

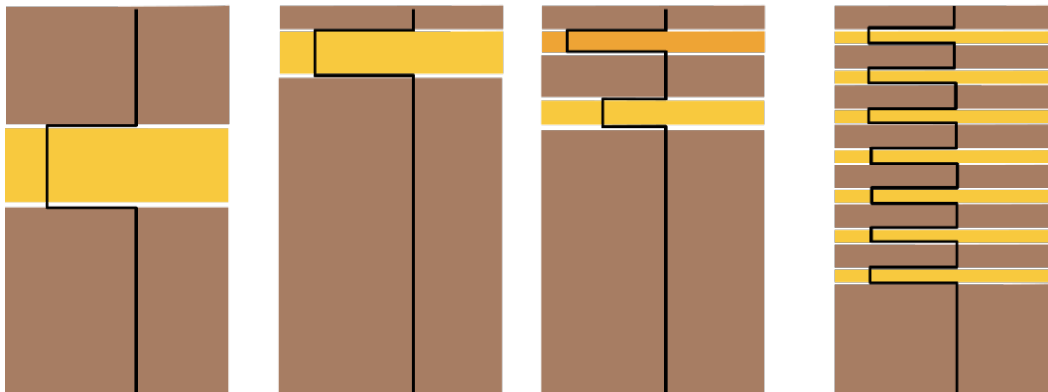
Combine the “damage” from structural deformation and rigid body movement

structural damage



Issues with single value definitions

CRR profile for LSN = 20 @ PGA = 0.15g



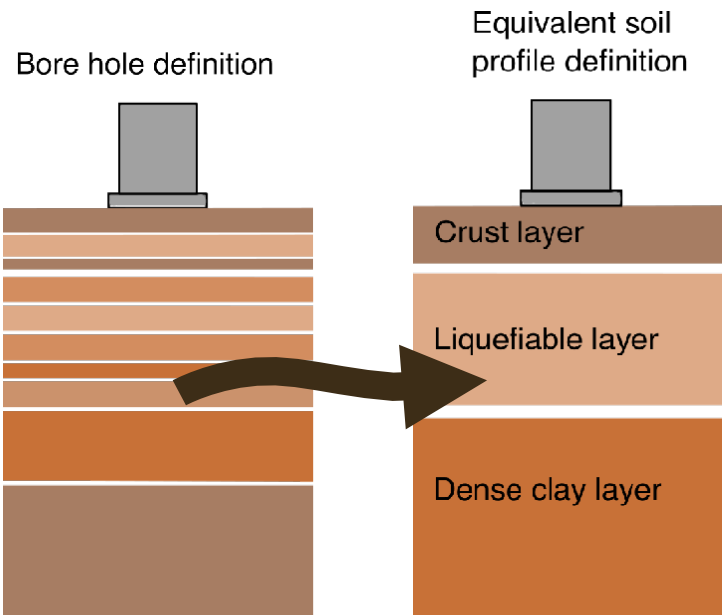
What level of differential settlement could be expected in the structure?

What level of shaking could be expected in the structure?

What level of soil-foundation stiffness could be expected?

- Difficult to validate for a single building as the soil profile is not uniquely defined
- Strong dependence on ground shaking
- Liquefaction can be beneficial and detrimental to performance

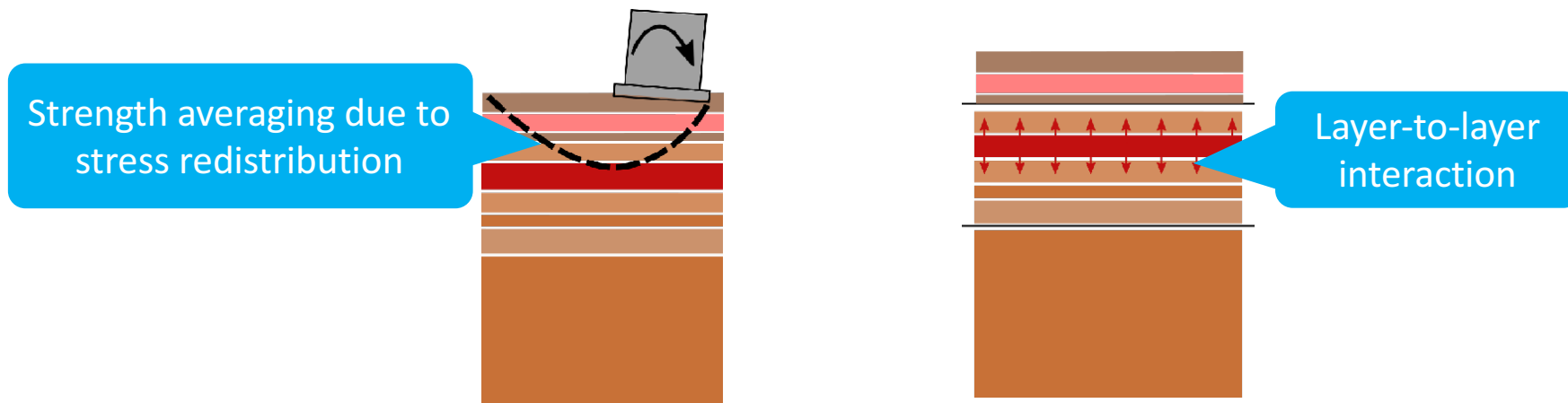
Why use an equivalent soil profile?

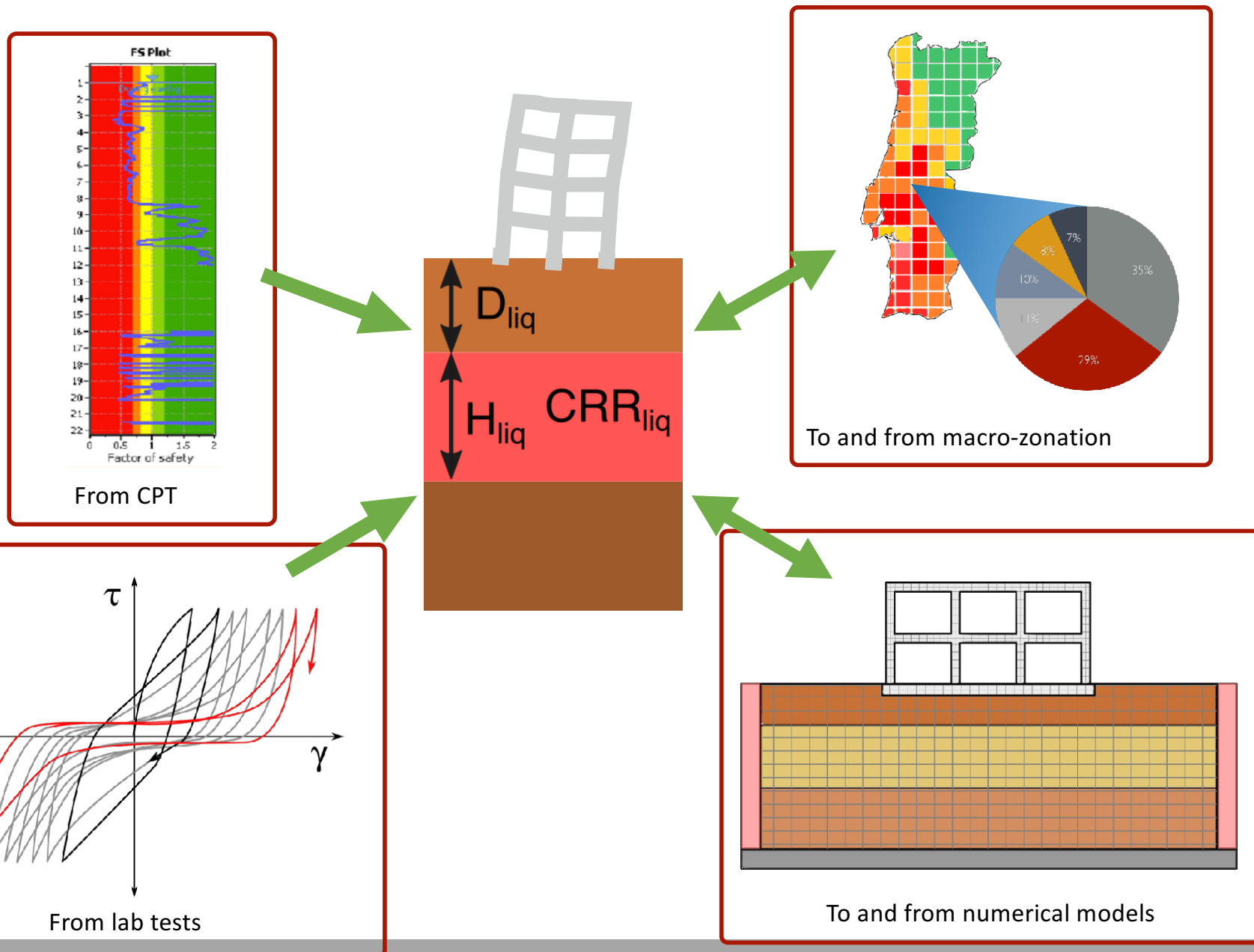


Practical reasons

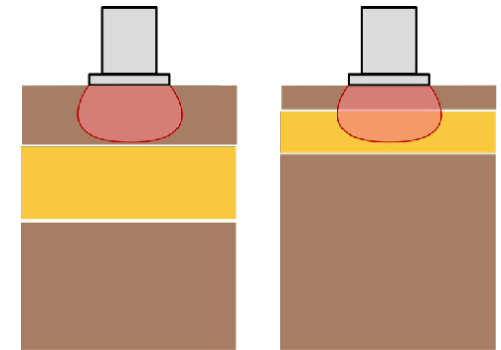
- Easier to understand the mechanics
- More intuitive
- Faster (less parameters)
- Connects with existing literature
 - Dimitriadi et al. (2017)
 - Bray and Macedo (2017)
 - Karamitros et al. (2013)
- Some level of equivalent layering has to happen.

Physical basis

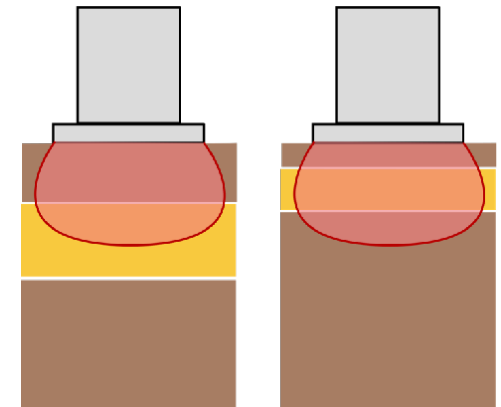
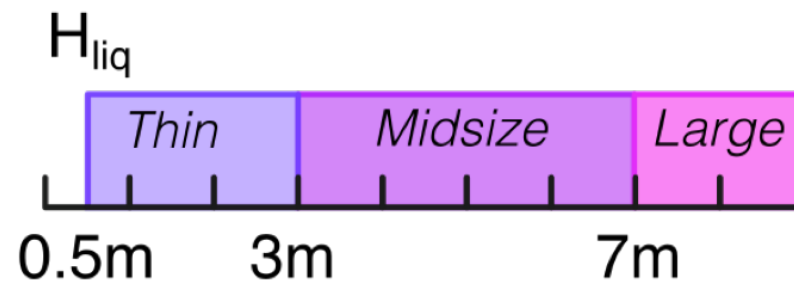




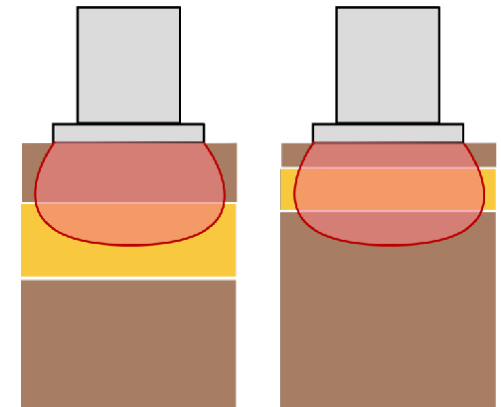
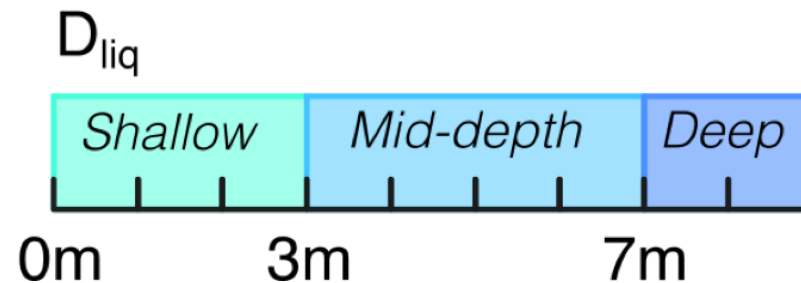
Proxy for time to liquefaction
based on shaking hazard



Proxy for change in ground
motion characteristics and
bearing capacity/settlement



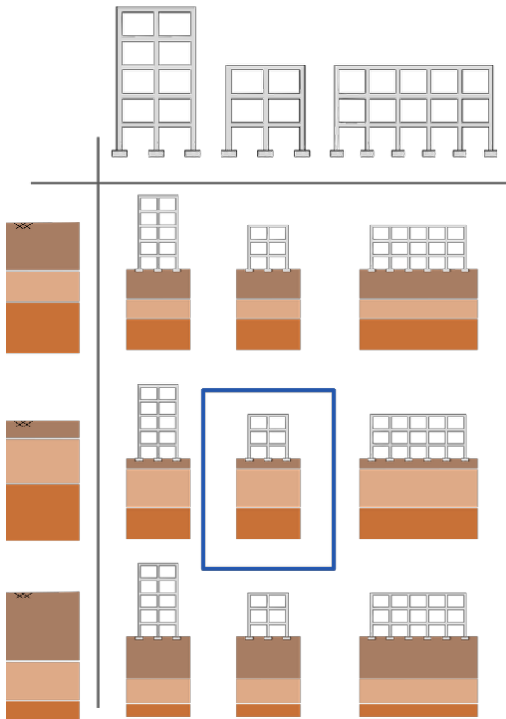
Proxy for change in ground
motion characteristics and
bearing capacity/settlement



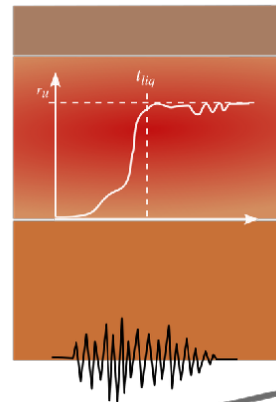
Strength - Size - Position

		Weak	Mid.	Strong	Resist
Large	Shallow	WLS	MLS	SLX	RXX
	Mid.	WLM	MLM		
	Deep	WLD	MLD		
Midsized	Shallow	WMS	MMS	SMX	
	Mid.	WMM	MMM		
	Deep	WMD	MMD		
Thin	Shallow	WTS	MTS	STX	
	Mid.	WTM	MTM		
	Deep	WTD	MTD		

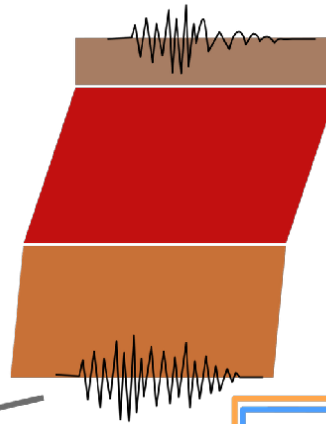
1) Select a building-soil class.



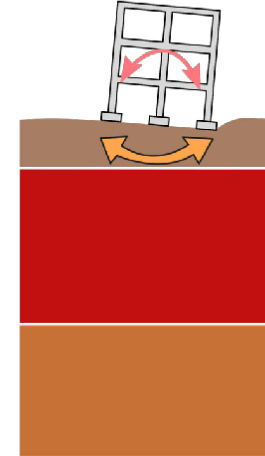
2) For a given ground motion, estimate time to liquefaction.



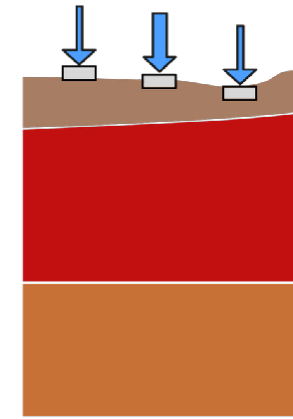
3) Estimate surface ground motion considering site response.



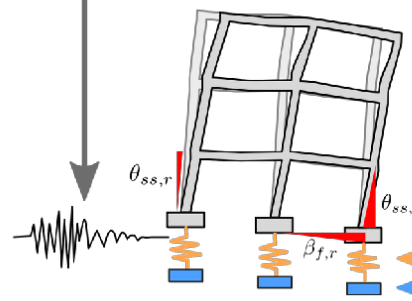
4) Estimate soil-foundation interface nonlinear stiffness.



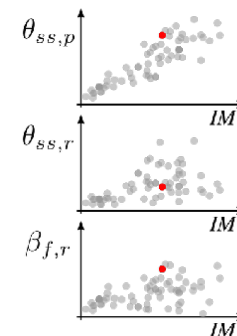
5) Estimate load-settlement and tilting relationships considering soil variability.



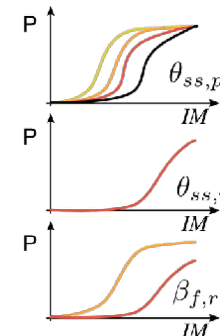
6) Analyse structural behaviour, considering SFSI, site response and settlement with load redistribution.



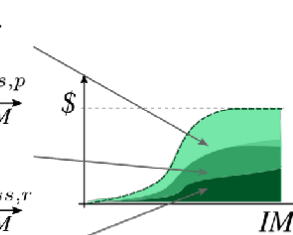
7) Determine the peak and residual drift and foundation rotation.

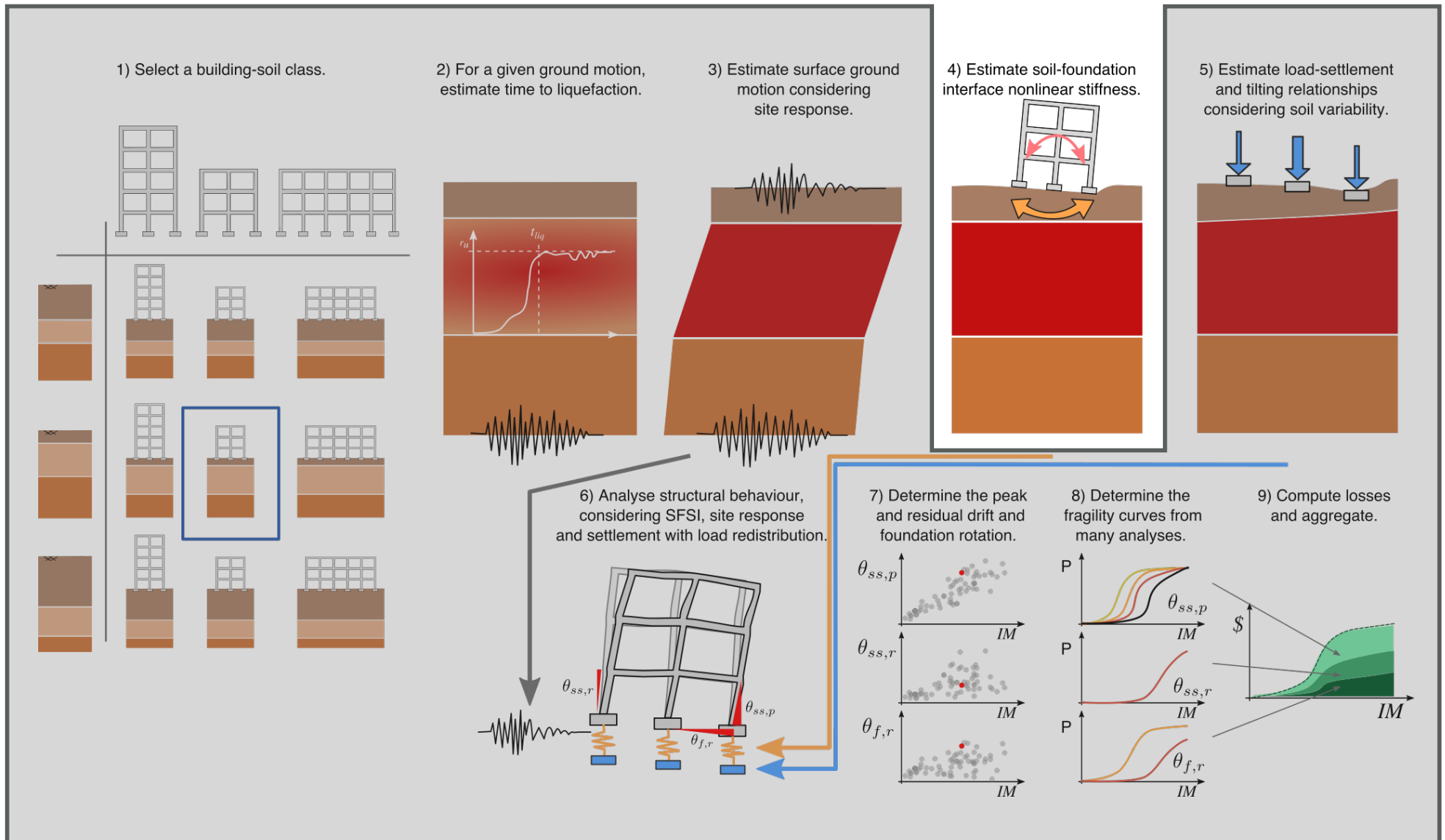


8) Determine the fragility curves from many analyses.

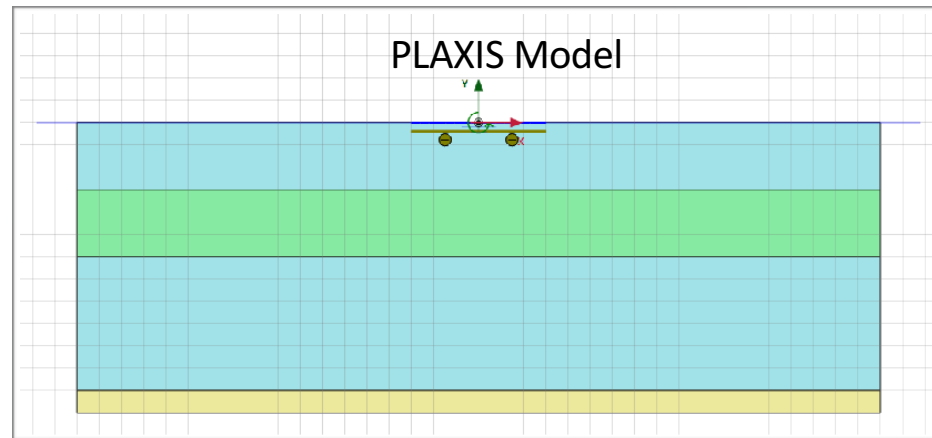
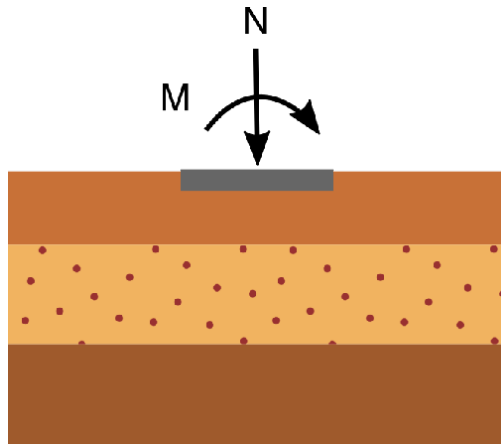


9) Compute losses and aggregate.

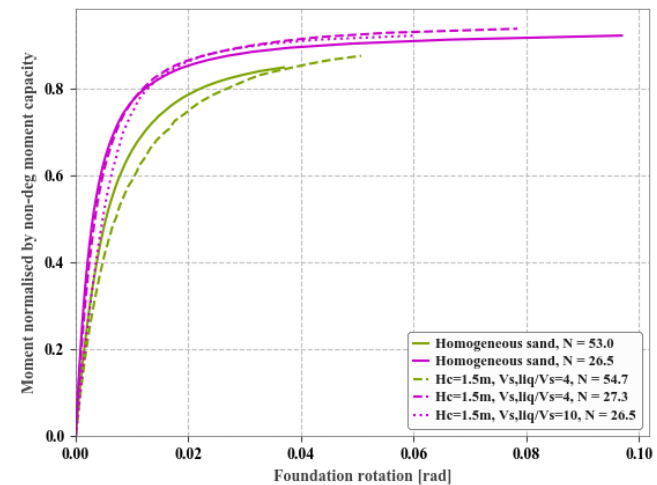
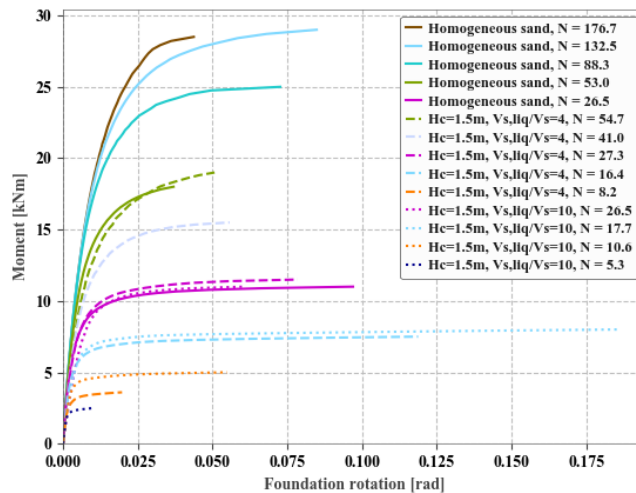


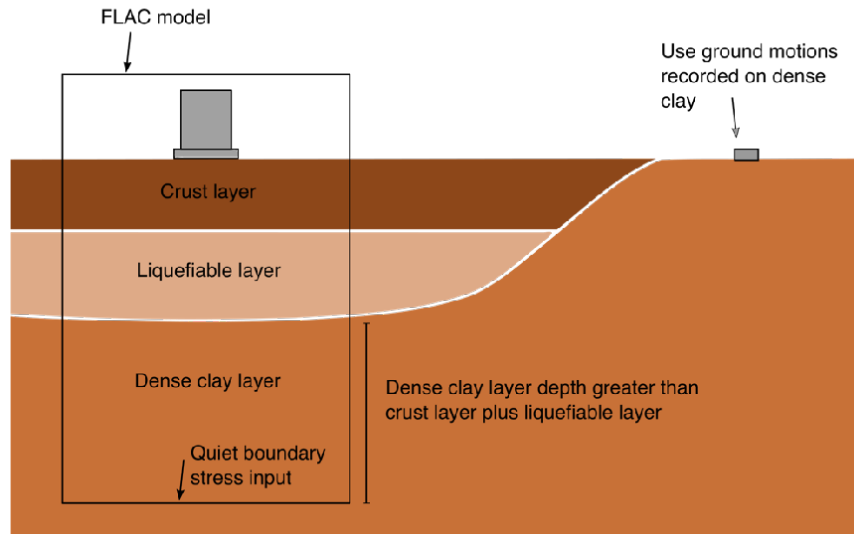


Extended study: Influence of liquefaction on non-linear foundation rotation



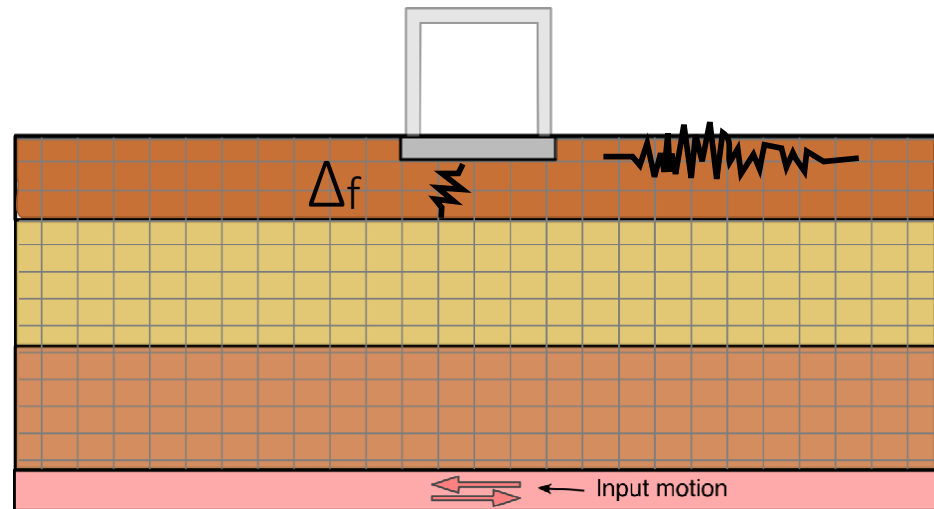
In many cases moment capacity is largely unaffected by liquefaction, but stiffness changes





Problem definition

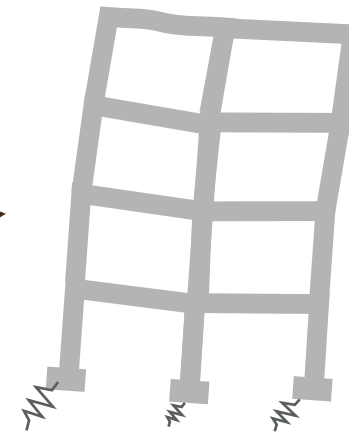
Model the soil system with a simple structure

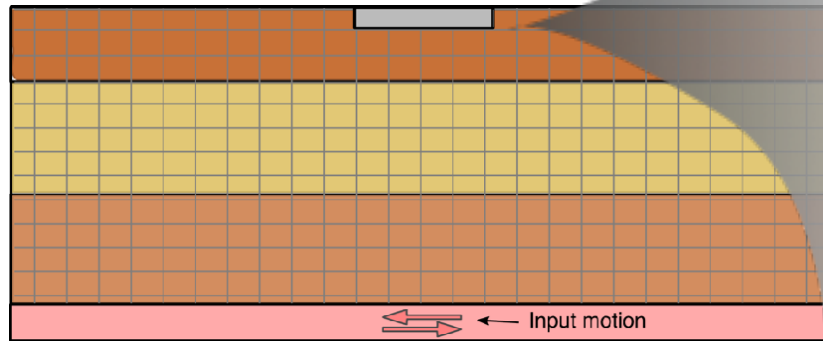


Extract time series of:

- Settlement
- Stiffness
- Surface shaking

Model the structural system





Relationship with N , to account for load redistribution

